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AND RELATED SUBJECTS

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#### TEXAS CALLING

#### bу

Prof. Frank A. Heacock, Chairman, Division of Engineering Drawing A.S.E.E.

All teachers of engineering drawing, descriptive geometry and related courses are cordially invited to the Drawing Division conferences, luncheon and dinner to be held during the annual A.S.E.E. convention at the University of Texas June 14-18, 1948. Our Executive Committee has planned a program which will be interesting and worth while. It is printed on page 5 of this issue of the Journal of Engineering Drawing.

Three features of the program deserve special mention. On Monday afternoon there will be a joint conference of the Drawing Division with the Machine Design group of the Mechanical Engineering Division. Our colleagues in these two groups have kindred interests and it is essential that we keep in close touch with each other in order to coordinate our teaching properly. Therefore, this joint conference promises to be of mutual benefit.

The Drawing Division conference on Wednesday evening has a special appeal for teachers who are interested in visual aids. Professor Charles E. Rowe of the University of Texas, whose collection of teaching models is regarded as one of the finest in America, will give a demonstration of his models at this conference.

The Teaching Clinic on Engineering Drawing and Descriptive Geometry, scheduled for Tuesday afternoon, is organized primarily to benefit young instructors who need counsel and guidance in their teaching problems, but it should be of interest and value to all of us who strive to improve our methods of instruction. A panel of competent and experienced teachers will be on hand and prepared to answer all questions. Teaching demonstrations at the blackboard will be given by an accomplished blackboard teacher. Ample time and opportunity will be allowed for general and specific questions and satisfactory answers, as well as appropriate discussion. It is our earnest hope that a large number of our colleagues, particularly the younger instructors, will attend this Teaching Clinic and take an active part in the proceedings.

Let us all get together and make this annual meeting a big success. I am looking forward to the pleasure of seeing you at Austin in June.

#### PRELIMINARY PROGRAM

Division of Engineering Drawing A.S.E.E. Annual Convention The University of Texas, Austin June 14-18, 1948

#### Drawing Division Luncheon

Monday, June 14, 12:30 P.M. Chairman, Frank A. Heacock, Princeton University Secretary, Orrin W. Potter, University of Minnesota Speaker, Edward M. Griswold, The Cooper Union Subject, "Engineering Drawing an Experience in Engineering"

Report of Nominating Committee, Justus Rising, Chairman, Purdue University

Election of Officers

Joint Conference of Drawing Division with Machine Design Group of Mechanical Engineering Division

Monday, June 14, 2:00 P.M.

Chairman, Frank A. Heacock, Princeton University Secretary, Ernst L. Midgette, Polytechnic Institute of Brooklyn

First Speaker, William H. Taylor, University of Alabama Subject, "Some Relationships between Descriptive

Geometry and Mechanics and Mathematics"

Second Speaker, Howell N. Tyson, California Institute of Technology Subject, "Preparing the Beginning Engineering Student in the Drawing Class for His Later Work in Machine Design"

Third Speaker, Alexander W. Luce, Pratt Institute Subject, "Standard Parts and Practices" Fourth Speaker, Stephen B. Elrod, Purdue University Subject, "Modern Dimensioning Practices"

Teaching Clinic on Engineering Drawing and Descriptive Geometry

Tuesday, June 15, 2:00 P.M. Chairman, Walter H. McNeill, University of Texas Secretary, Orrin W. Potter, University of Minnesota Blackboard Demonstrator, Henry C. Spencer, Illinois Institute of Technology

Members of Panel to be announced later

#### Drawing Division Dinner

Wednesday, June 16, 6:00 P.M. Toastmaster, Walter H. McNeill, University of Texas Secretary, Orrin W. Potter, University of Minnesota

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Speaker, Carl L. Svensen, Secretary-Director, Texas State Board of Registration for Professional Engineers

Subject, "Drawing in Engineering Education"

#### Drawing Division Conference

Wednesday, June 16, 8:00 P.M. Chairman, Frank A. Heacock, Princeton University Secretary, Orrin W. Potter, University of Minnesote First Speaker, Charles E. Rowe, University of Texas Subject, Demonstration of Models

Second Speaker, Paul M. Mason, A & M College of Texas Subject, "An Adaptable Teaching Model for Orthographic Views"

Third Speaker, E.G. Kirkpatrick, Purdue University Subject, "A Rating Scale for Grading Engineering Drawings" Reports of Committees

Other Business

#### **TEXAS WELCOMES YOU**

#### by

James D. McFarland Associate Professor of Drawing The University of Texas

To the members of the Drawing Division of A.S.E.E., The University of Texas extends a hearty welcome. It will be a privilege to have you as our guests, and we hope to make your visit so enjoyable that you will decide to see more of our city and state after the convention has ended.

Austin, "the friendly city", and home of The University of Texas, may be reached by any of the wellknown modes of transportation. The Missouri-Kansas-Texas Railway gives passenger service through the "Texas Special," and the Missouri Pacific Railway gives special passenger service through the "Sunshine Special." These two trains have a 22-hour service to St.Louis and 45-hour service to New York City. The Southern Pacific Lines offer excellent passenger service to all Southern, Western and Eastern points.

The Southwestern Greyhound Lines, Inc., Bowen Motor Coaches, and Kerrville Bus Company, Inc., furnish motor bus transportation in all directions.

High-speed transportation is furnished by several air lines which use the Robert Mueller Municipal Airport as a terminus. Austin is on the regular passenger, mail and express line between San Antonic and Dallas, and has connections with all other points.

If you plan to drive to the meeting then you will have a better opportunity to view the rolling hill country, the beautiful lake region and other spots of interest in and around Austin. The following highways pass through the city: U.S. 79, U.S. 81, U.S. 290, Texas 2 (Same as U.S. 81), Texas 20, Texas 29, Texas 43, Texas 71, Texas 165.

Within a radius of 60 miles of Austin there are five lakes with a combined shore line in excess of 600 miles. Lake Austin is within the city limits and Lake Travis, formed by the huge Mansfield Dam, is only 17 miles from the heart of the city. All Texas is proud of this chain of lakes, and the mountainous and wooded sections surrounding them contain an abundance of deer and wild turkey. Fishing in the lakes is excellent.

In and immediately adjacent to the city you will find recreational facilities of most every kind. Zilker Park provides swimming, horseback riding, picnic tables, and several miles of roadway in the hilly section overlooking the Colorado River. Swimming is also available at Deep Eddy Bathing Beach. If you play golf you will find accommodations at the Municipal Golf Links or the Austin Country Club Links. Tennis courts are in abundance at the University campus and will be at your disposal. Good fishing may be had all around Austin.

Within the city are many points of interest. Among these are the Governor's Mansion, Elisabet Ney Museum, Texas Memorial Museum, Mt. Bonnell, the home of O'Henry, the Treaty Oak and others too numerous to mention. Austin has the unique distinction of being the only city in the world lighted by "artificial moonlight". This is accomplished by the tower lights lights of 9,600 candlepower on top of 165 ft. steel towers - scattered about the city.

Courses in engineering were first given at The University of Texas in 1894. Since that time well over 3000 degrees in the various branches of the profession have been conferred. Degrees are offered in eight branches of engineering and in Architecture. The current enrollment in the College of Engineering is 3,681 students.

The Main Campus of The University covers about 200 acres. We have many fine buildings which we would be happy to show you, and some temporary wooden ones erected this past summer that will probably remind you of some which you, too, have had to use in order to take care of the heavy post-war enrollment. There are 17,343 students in attendance at the Mair University this semester.

Housing accomodations for you are available at hotels, tourist courts, and dormitories. Most of these are within two miles of the compus.

Meals, other than those scheduled, may be had on or near the campus or down town. Prices are reasonable.

Entertainment has been provided for everyone. Arrangements have been made to take care of children if this service is desired. (Continued on page 14)



## WITH A LIGHT THAT CANNOT BE SEEN

Photo courtesy Radio Corporation of America

AMERICAN SOLDIERS in pitch dark able to see clearly the enemy ahead; scout cars speeding at 50 miles an hour along blacked out roads in perfect safety; officers of the law seeing clearly the operations of hijackers "hidden" by night: these are some of the miracles performed with the help of the infrared telescope. Workers in the dark are thus aided by a light that cannot be seen.

It can be said that young lads, on the way to take their place in the world, possessed of hungers for they know not what, driven by innate energies they know not where... are just as truly working in the dark. And so, too, educators must illuminate the obscure face of the future for them ... using a light that cannot be seen, the light of searching and sympathetic wisdom. Only then can a boy establish a goal that is socially useful and a personal recompense. Only thus can stumbling feet be kept on the road.

And how can the educator's responsibility be discharged, how can the unseen light be effectively used, if not with and through the familiar things of school routine? For example, the drawing instruments a youngster will use when he comes to mechanical drawing class... their very selection can be an opportunity which gives a momentary glimpse into the beyond. These are tools of engineering, and engineering is the great hero of today and tomorrow. Shall its very instrumentality be chosen carelessly, treated with equal disregard? Or can the fact of great achievement be reflected into the life of the youngsters by a beautiful set, an exquisitely wrought set, a set to proudly possess the rest of the student's life... a set that may well be a touchstone, the source of another light that may also help to lead the lad onward and forever upward? Upon the right selection here vital values rest.

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## AN APPLICATION OF ADVANCED GRAPHICS: CRYSTALLOGRAPHY 1

by

Howard T. Evans, Jr. Section of Graphics, Massachusetts Institute of Technology

#### INTRODUCTION

Nowadays we are beginning to appreciate the value of graphics as a tool of science, and realize that graphical mathematics is a science itself, a well defined branch of mathematics. That graphics has not been recognized as a science, as mathematics has been, is a great pity, for each of the sciences has had to develop its own graphical methods empirically. This is a process which has generally been rather inefficient, because, under these conditions, the graphical methods are considered secondary to the problems to which they are applied, and hence have not been subjected in many cases to intensive development. This situation has been clearly pointed out by John T. Rule<sup>2</sup> in an article in which he urges that the science of graphics be recognized and developed to serve other sciences in the solution of problems for which up to now these sciences have been using make makeshift methods.

In the paper by Rule just mentioned, there is a reference to crystallography as an example of one of the sciences in need of highly developed graphical methods. It so happens that crystallography is one of those sciences which has realized the power and indispensibility of such methods and has indeed developed them to a very high degree. The science of crystallography might stand as a model for the manner in which graphics has been applied. On the other hand, unlike most other sciences, crystallography has made rather poor use of algebraic mathematics, preferring rather the graphics. It is the purpose of the present paper to describe some of the graphical methods of crystallography and to illustrate the great power of such methods.

The crystal, as a body bounded by plane faces, very early attracted the attention of graphically minded men. It was not until about 1800, however, that the naturalist Hauy discovered that unlike Nature's other graphical expressions, crystal forms are rigidly defined mathematically on the basis of a regular internal periodicity of structure. Following this discovery, crude graphical and mathematical methods were developed for measuring and defining crystals. Since the form of a crystal is characteristic of the substance of which it is composed, drawings of crystals were found to be very valuable in the descriptions of minerals and chemical compounds. Around 1880, V. Goldschmidt began making his contributions to graphical methods of crystal measurement and drawing. Goldschmidt brought about a revolution wherein makeshift methods were replaced by fundamental methods. It may be said that the present state of graphical crystallography is the result almost entirely of the work of this one man.

In 1912, it was found by von Laue that X-rays could be diffracted by the periodic structure of a crystal, just as light is diffracted by a ruled grating. Physicists and mathematicians at this point started studying this phase of crystallography. Because of the interplay of the different sciences, the mathematical state of crystallography has been tremendously improved in recent years.

Crystallography today thus is divided into two broad subdivisions, which are, of course, closely interrelated: crystal morphology, the study of the external form of crystals; and X-ray crystallography, the study of the internal structure of crystals. In the former, the single crystal is measured with an arm protractor or by more refined methods, represented graphically by certain types of projections, and characterized by the properties of these projections. In the latter, the crystal is bathed in a beam of X-rays, the diffracted beams recorded on photographic film, and the resulting data combined by various graphical and mathematical means to yield the structural constants of the crystal, and ultimately, the precise locations of all the atoms in the crystal. The graphical methods in the process of X-ray analysis of crystals are among the most powerful and magnificent ever developed in any field, but unfortunately, these lie be-yond the scope of this paper. Here we must confine ourselves to crystal morphology, and survey the methods developed by Goldschmidt and his followers. These methods involve the problems, familiar to us, of measuring angles and lengths in space, and projecting solid bodies orthographically onto planes.

<sup>1</sup>Presented at the Annual Convention of the A.S.E.E. at Minneapolis, Minnesota, June 1947. <sup>2</sup>John T. Rule, "Graphics Re-examined", J. Eng. Draw., Feb. 1947, pg. 1.

#### ANALYTIC GEOMETRY OF CRYSTALS

No chestra

Since crystals are bounded by plane faces, it is natural to refer these planes to three axes in space and define them by their intercepts on these axes. The axes in general will not be Cartesian, but may be inclined, and measured with different scales. The choice of axes will depend on the symmetry of the crystal being measured; the interaxial angles  $\alpha$ ,  $\beta$  and  $\gamma$ , and axial scales, linear in the ratio a: b: c, depend on the substance forming the crystal and are characteristic of that substance. When a crystal face is extended to intersect these three axes, three intercepts will be determined; as the crystal grows, these intercepts will change, but their <u>ratio</u> re-mains constant. If the interaxial angles and scales are properly chosen, it turns out that this ratio may always be expressed by simple whole numbers ("Law of Rational Intercepts").

For many decades, crystals were treated directly in this way, and the characteristic interaxial angles and scales were, related to the dihedral angles between faces by brute force spacial trigonometry or elementary analytic geometry. When crystal drawings were made, the three axes were set up in pictorial form by a method known as the "clinographic" projection. The intercepts of each plane were laid off on the projected axes, and the intersections of the planes determined from their traces on the axial planes; thus the crystal was built up edge by edge. If the crystal was at all complex, the trigonometry and crystal drawing by axial intercepts became very tedious and trying. Clinographic projection was described in the fifth edition of Engineering Drawing by French, but has been wisely omitted in recent editions.

#### PROJECTION METHODS

Crystals being solid bodies, they are characterized by three dimensions. The three dimensions for any crystal face may be defined as follows: the strike of the face (azimuth angle); the dip of the face (inclination angle); and the distance of the face from the origin. From our discussion, we have seen that the internal structure of the crystal determines the first two of these dimensions; thus the dihedral angles are strictly controlled. But the last dimension is not dependant on the crystal structure, but on the rate of growth of the face, which varies with many factors of circumstance. . Thus, the mathematical definition of a crystal, as an expression of its internal structure, is concerned with only two dimensions, the first two listed above. The dihedral angles between faces are a function of these two dimensions and therefore are of prime importance; but the shapes and sizes

of the faces depend on the third, and have no significance for our present purpose.

These considerations suggest that there may be some convenient way of representing the two dimensions we are interested in on a two-dimensional surface, the plane of the paper. Actually, two such graphical transformations, the gnomonic and stereographic projections, have been found very useful. We shall now see how each is derived and what briefly are their properties. Many readers are no doubt familiar with these same projections as used in other fields, aspecially cartography, but their application to crystallography is particularly dramatic.

If we establish an origin somewhere near the center of the crystal, we may erect at this point a line normal to each face on the crystal. Each of these vectors will have dimensions equivalent to those of the face, angle of azimuth and angle of inclination; if the length of the vector is not limited, the third dimension remains undetermined, in accord with our plan. Each face on the crystal will then have a corresponding perpendicular, and we may think of the crystal in terms of these two-dimensional vectors alone. Now, suppose that a sphere of unit radius is drawn with its center at the origin. As shown in Figure 1, each vector will pierce the surface of the sphere in a point. The crystal is thus transformed into an arrangement of points on the two-dimensional surface of the sphere, each point p representing a



Fig. 1. Construction for the spherical, gnomonic and stereographic projections.

crystal face p. If a convenient coordinate system is set up, the position of each point can be measured in terms of two angles corresponding to the longitude and latitude angles used to measure the position of points on the earth's surface. The azimuth angle is designated  $\phi$ , measured from 0° to 360°, and the inclination angle p, measured from 0° to 180°. The latter, corresponding to latitude, is measured from the north pole, instead from the equatorial plane.

(Continued on page 21)

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#### A GRAPHICAL SOLUTION FOR

## THE REDUCTION OF TWO NON-INTERSECTING NON-PARALLEL FORCES IN SPACE

#### by

E.J. Marmo Associate Professor of Engineering Mechanics University of Nebraska

When a rigid body is subjected to the action of forces which are directed so that they are neither parallel nor intersecting, the problem in the analysis of external force action can be resolved into one of four possibilities, depending upon the magnitude, direction and point of application of the forces. The reduction may result into:

- (1) A single force
- (2) A single torque or couple
- (3) A system of force in equilibrium
- (4) A force and a couple

The first three possibilities represent conditions which will exist for special cases only. The fourth possibility is one which covers the general cases and is to be the one which concerns the discussion which follows.

Regardless of how complicated the force system may be in dealing with non-concurrent and non-parallel forces in space, these forces are the equivalent to a single resultant force and a single resultant torque. If the torque can be made to act at right angles to the direction of the forces we have the simplest case in the reduction - a wrench.

The use of graphical solutions has been extensively used by the designer in analyzing the external force actions on bodies. It seems that this type of a solution has been restricted mainly to forces which lie in a single plane. Some use has been made of graphical solutions dealing with problems having concurrent forces in space.

The application of graphical solutions to problems dealing with non-intersecting non-parallel forces in space has been very much neglected. It is my belief that with a proper knowledge of mechanics combined with a proper knowledge of the principles of descriptive geometry considerable time and effort can be saved by the engineer if he resorts to graphical solutions for problems of this type.

In order to more fully appreciate the possibility of using the graphical solution in preference to the analytical solution it might be of interest to briefly outline the steps involved in a mathematical solution.

The two forces AB and CD act on a rigid body as shown by Fig. 1. AB has a magnitude of 2310 lb and bears N54° 30'E with a slope of 28° 10' below the horizontal. CD has a magnitude of 1655 lb and bears N39° 15'E with a slope of 9° below the horizontal.

- 1. Select any convenient point such as A and draw the x, y and z axes through that point.
- 2. Resolve the force CD so that it will consist of a parallel force AD<sub>1</sub> through the



- 3. The force system now consists of two concurrent forces AB and AD<sub>1</sub> and a couple made up of the two equal and opposite parallel forces CD and AD<sub>2</sub>. The external effect on the body caused by this new arrangement of forces remains unchanged from the original condition.
- 4. Find the resultant of the two concurrent forces AB and AD<sub>1</sub> by resolving each force into components parallel to the x, y and z axes. Then find  $\bowtie F_x$ ,  $\nvDash F_y$ ,  $\limsup F_z$ . The resultant can be determined by the equation  $R = \sqrt{\varkappa F_x^2 + \varkappa F_y^2 + \varkappa F_z^2}$ .
- 5. Find the angle that the resultant makes with the x, y and z axes. If the angles which the resultant makes with the x, y and z axes are respectively  $\alpha$ ,  $\beta$ , and  $\beta$ . The angles are derived from the equations.

$$\cos \alpha = \frac{\Xi F_x}{R}$$
$$\cos \beta = \frac{\Xi F_y}{R}$$
$$\cos \beta = \frac{\Xi F_z}{R}$$

- 6. In general the couple determined by the two equal and opposite parallel forces CD and AD<sub>2</sub> will not cause rotation at right angles to the resultant force R passing through the origin.
- 7. The direction of the plane of the couple can be determined by finding the angles which the normal to this plane, passing through the origin, makes with the x, y and z axes. The normal to the plane is also the vectorial representation of the couple. It is explained in Fig. 4.

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8. For the general case the vector representation of the couple and the resultant force vector R do not make the same angles with the x, y and z planes. It then becomes necessary to combine the two vectors so that the couple lies in a plane perpendicular to the force R. The position of R has to be displaced parallel to itself in order to meet this condition.

The procedure outlined above is one analysis for arriving at the reduction of forces in space which are non-concurrent and non-parallel. The condition to which it reduces the forces is one in which we have translation along one line such as F and a minimum torque M<sub>R</sub> in a direction at right angles to the line. This condition is shown by Fig. 2. It can be seen



from the preceding steps that there are numerous space relationships which involve the use of trigonometry and algebra. The work becomes very tedious and for this reason such problems can often be solved more readily with the use of a graphical method.

#### GRAPHICAL SOLUTION

The application of descriptive geometry to the solution of the same problem that has been previously mentioned is shown by Fig. 3.

- GIVEN: Two forces AB and CD acting at given distances on a rigid body. The 2310 lb force AB applied at point A has a slope of  $28^{\circ}$  10' below the horizontal and has a bearing of N54° 30'E. The 1655 lb force CD applied at point C has a slope of 9° below the horizontal and has a bearing of N39° 15'E.
- REQUIRED: The reduction of these two forces which are non-parallel and non-intersecting to their simplest form; namely, a single resultant force and a single resultant torque as shown by Fig. 2.

ANALYSIS: (1) The two given forces AB and CD are represented by vectors in the top and front view of Fig. 3 according to the specified directions and to a specified scale.

(2) Through any convenient point on AB, such as A, draw two equal and opposite force vectors, AE and AF, parallel to and equal to CD. This is

done in both the top and front views. The external effect on the rigid body has not changed due to this transposition.

(3) The composite vector forces acting on the rigid body can now be considered to be made up of two concurrent vector forces AB and AE and a couple represented by the two vectors CD and AF which are opposite in sense and parallel to each other.

(4) AG the resultant of the vector force AB and AE is determined by the use of the parallelogram of forces shown in the top and front views.

(5) The auxiliary view taken adjacent to the front view is drawn in the direction of a frontal line CM of the plane of the couple (two parallel force vectors) and it shows the plane of the couple appearing as an edge. This view is labeled with the subscript  $A_1$ .

(6) The oblique view labeled with subscript O<sub>1</sub> is taken from the auxiliary view (A<sub>1</sub>) in a direction perpendicular to the plane of the couple. This view shows the true length of the force vectors making up the couple and it also shows the true distance between the vectors. This scaled distance (1.78 in.) times the magnitude of the force vector  $C_{O_1} D_{O_1}$  or  $A_{O_1} F_{O_1}$  (1655 1b) gives the moment of the couple (2950 1b'in.)

(7) The oblique view labeled with the subscript  $O_2$  is taken from the oblique view  $(O_1)$  in a direction perpendicular to the resulant  $A_{O_1} G_{O_1}$ . This view shows the plane of the couple appearing as an edge and it also shows the true length and true angle that the resulant AG makes with the plane of the couple.  $A_{O_2} G_{O_2}$  has a magnitude of 3890 lb and makes an angle of  $12^{\circ}$  with the plane of the couple

determined by the vector forces  $C_{O_2} D_{O_2}$  and  $A_{O_2} F_{O_2}$ .

(8) The next step involves the representation of a couple by a vector. Fig. 4 shows an example of how this is done. If two forces such as  $F_1$  and  $F_2$  form a couple the magnitude of the couple is  $F_1$  or  $F_2$  times y. If  $F_1$  is in pounds and y is in inches the magnitude is in 1b in. The magnitude of this couple can be represented by a vector V by drawing to a definite scale (representing 1b in.) a line which is perpendicular to the plane of the couple and which is directed so that it projects outward from the view of the plane which shows the couple action appearing in a counterclockwise direction.

(9) Referring to Fig. 3 again, and to the oblique view  $O_2$ , the couple having a magnitude of 2950 lb in. is represented by the vector  $A_{O_2} = J_{O_2}$ .

(10) With the use of the triangle of forces, the vector  $A_{O_2} J_{O_2}$  is resolved into two components, a component  $A_{O_2} H_{O_2}$  in a direction collinear with the resultant force  $A_{O_2} G_{O_2}$  and the other component  $H_{O_2} J_{O_2}$  in a direction perpendicular to the result-

ant. The magnitude of AH equals 625 lb in. and the magnitude of HJ equals 2885 lb in.





F16. 3

(11) The oblique view Og is taken in a direction perpendicular to the resultant AG in the oblique view Og. In this third oblique view the resultant AG still appears in its true length. The couple vector AH is also in its true length in this view and still collinear with AG. The couple vector HJ having a magnitude of 2885 lb in. is resolved back into two forces  $A_{O_3} \times_{O_3} K_{O_3}$ 

parallel to each other and opposite in sense. AK is equal to and collinear with AG but opposite in direction. The distance of 0.74 in. is determined so that the magnitude of the couple represented by the vector HJ (2885 lb in.) could be obtained by two forces AK and LN each of which is equal in magnitude to AG. In other words the magnitude of HJ (2885 lb in.) divided by AG (3890 lb) is equal to 0.74 in.

(12) The condition which now exists in the oblique view  $\Omega_{\rm S}$  is one in which two equal collinear forces



AG and AK cancel out because they are opposite in sense. This leaves the two vectors LN and AH. LN, by construction, is equal to AG and therefore equal to 3890-1b. The direction of LN is also unchanged from that of AG but the point of application has changed. AH is the vector representation of a couple and is equal to 625 lb in. The plane of the couple representing AH is perpendicular to the direction of the vector IN. This reduction brings about the simplest form of the two original forces AB and CD. It is evident from the foregoing discussion and the accompaning solution that the application of descriptive geometry offers a splendid opportunity for arriving at a rapid solution for problems dealing with the analysis of force action in space. The accuracy attained will naturally depend upon the precision in the workmanship and also upon the selection of suitable scales. It will conform to the same degree of accuracy that the graphical solution has to a mathematical solution for problems dealing with forces lying in one plane.

#### NEWS

Professor Hoelscher informs me that the manuscript of the proceedings of the 1946 summer school are now in his hands. The material is to be re-edited for possible publication this coming fall.

#### \*\*\*\*\*

An institute for effective teaching has been established at the University of Detroit through the effort of Dean Clement J. Freund of the College of Engineering, as a means of aiding faculty members at giving a maximum of instruction in the classroom.

Among the members of the faculty asked to lecture at these meetings is Jasper Gerardi, Assistant Dean of the College of Engineering and Chairman of the Department of Engineering Drawing.

\*\*\*\*\*

Fred Higbee and John Russ of Iowa suggested a "new equipment" or "what's new and interesting" department in the Journal of Engineering Drawing. Submit any interesting items that you wish to bring to the attention of the Editor of the Journal.

\*\*\*\*\*

A General Engineering Department has been organized at the University of New Mexico. Professor J. Humerich is head of the department. This department teaches courses in Engineering Drawing, Descriptive Geometry, Orientation, and Engineering Problems.

\*\*\*\*\*\*

It is nice to receive an occasional word of commendation from men outside your immediate field of endeavor. In a recent letter to the editor, Dean G.N. Butler, of the University of Arizona, wrote:

I looked over the contents of your magazine with much interest and approbation. I do not see how a drawing instructor can get along without it.

Professor Paffenbarger and his committee on advanced credits are to be congratulated on doing a fine job and a big job in so short a time.

Professor Street writes:

We have recently had two graduate courses in drawing approved at this institution and they are as follows:

- 601. Advanced Industrial Drawing. (2-2) Credit 3
- 603. Advanced Machine Drawing. (1-5) Credit 3

These courses will be given the first term of summer school during 1948 which runs from June 7 to July 17, 1948. They will be repeated from July 19 to August 28, if there is sufficient demand. This makes it possible for people to take a minor in drawing at Texas A.& M. College doing graduate work.

#### \*\*\*\*\*

How many of you have requested copies of the tests made available by the Committee on Advanced Credits? If you have not asked for copies to assist in the validation of these tests, you should do so soon. You can receive these tests by writing to:

The Project Office 437 W 59th Street New York 19, New York

#### \*\*\*\*\*

During the past two years, Professor Francis Porter of the University of Illinois has submitted problems, and served as a committee of one in making a selection of the best solutions submitted to the problems, in the Journal under the title of "Solve This One." As Editor, I want to thank Professor Porter for the fine job that he has done.

#### (Continued from page 6)

It is particularly desirable that there be a good attendance of the younger members in the drawing field. We extend to them a special invitation and hope that you older members will urge the youngsters of your department to attend the convention.

The program arranged by the Drawing Division is a good one and should be of great benefit to us all. We at the University of Texas are grateful for this oppertunity to renew old friendships and make new ones, and to return some of the hospitality that has been shown us elsewhere.

#### TEACHING TOLERANCES

bγ

J. Gerardi and E.J. Massard Department of Engineering Drawing University of Detroit

#### SPECIFICATION OF SURFACE ROUGHNESS

In the preceding articles of this series, methods of limit dimensioning were introduced in an attempt to show what can be taught to freshman and sophomore engineering students. This is the third and final article of this series.

Unfortunately, at present, there is no accepted standard in this country for the designation of surface roughness, particularly with reference to very close limits. While there has been a considerable change in drafting practice since the war, little or nothing has been done as to the specification of the quality of a machined surface. As a result, various manufacturers of machinery and equipment have adopted their own standards. Since the manufacturers are not using the same nomenclature for surface finish, confusion and misunderstanding exists. It is the purpose of this paper to present the trend in specifying surface limitations on drawings.

It has been found desirable to specify the required finish of critical surfaces on detail drawings in at least one of three ways.

- 1. A general note in the lower righthand corner of the drawing.
- 2. In the bill of material.
- 3. Along the edge view of the surface which is to be finished.

Before we can visualize the importance of surface specification, it is necessary that we have a clear understanding of the fundamental terms.

Surface Quality or surface roughness is the term used to designate characteristics of surface.

Nominal Surface is a two dimensional surface separated from a smooth shape from the surrounding medium. For example: The optional flat is the nearest approach to its nominal surface since it can be made to approach a plane so closely that departures from it are not measurable by any means known at the present time.

<u>Surface Deviation</u> is the departure of the actual surface of an object from the nominal surface of that object. For example: roughness, waviness, and surface flaws are surface deviations. Surface Flaw is the irregularity of any sort which occurs at only one place or at relatively frequent and widely varying random intervals in a surface. A surface flaw may be a scratch, a ridge, a hole, a peak, or a crack.

Waviness is a surface deviation which consists of irregularities in the form of a wave. On smooth machine surfaces, the length between each wave is ordinarily between .04 and .10 inches and the height of the waves is generally between .002 and .005 inches. Waviness can be measured by conventional dial indicators.

Roughness is the recurrence of irregularities in a surface ranging from .0002 to .010 inches between crests and from .005 to .010 inches in height.

<u>Microinch</u> is one millionth (.000001) part of the U.S. standard linear inch. The microinch is a unit of length convenient and appropriate to many measurements of roughness on "smooth machine surfaces."

Theoretical Root Mean Square (R.M.S.) is the square root of the sum of the squares of the values being averaged, divided by the total number of values. For example, in Figure I the root mean square value of the ordinates of the curve shown would be calculated as follows:



 $RMS = \sqrt{A_i^2 + A_a^2 + A_a^2} \dots N^2$ 

Figure I

Since it is impossible, at the present time, to measure the ordinates on a smooth surface, a profilometer is used to determine an average value of each root and crest in a wave. A profilometer is a very sensitive instrument containing a small diamond point detector. This detector is connected to a receiving unit which measures small changes in current, produced by the irregularities in the surface. A dial calibrated in microinches records the approximate root mean square value of the ordinates.

(Continued on page 32)

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This new edition adds several new chapters, many new illustrations, and a large number of problems reflecting present-day practice. A considerable amount of the old material has been revised, drawings have been changed where necessary to eliminate duplications and ambiguities, and the fundamental chapters I to X have all been revised to improve the order and to achieve clearer, more logical explanations.



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By GEORGE J. HOOD, Professor of Engineering Drawing, University of Kansas. Third edition, 362 pages. \$3.00

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By FRANK M. WARNER, University of Washington. Third edition, 252 pages, 5½x8½. \$2.75

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### PROBLEM SOLUTION

#### by

#### Melvin Hainey University of Texas

PROBLEM: Given any two non-parallel, non-intersecting lines, AB and CD. To construct a line MN terminating in them, and making specified angles  $\infty$  and  $\emptyset$  respectively with them.

ANALYSIS: The required line or lines will be parallel to the common elements of two right circular cones set up according to the following conditions: 1) the cones have a common vertex; 2) the axis of one cone is parallel to AB and its elements make the required angle with AB; 3) the axis of the other cone is parallel to CD and its elements make the required angle with CD.

CONSTRUCTION: Pass plane 12C through CD parallel to AB and obtain a normal view of this plane. In the normal view, the cones may be set up with their common vertex at any arbitrary point, such as B, and with equal slant heights. Draw lines connecting the common vertex to the points where the bases of the cones intersect. These lines are elements common to both cones and have the required directions for the solutions. The actual connecting lines may be obtained from an adjacent view which is an end view of either one of the lines, AB in this case.

DISCUSSION: The drawing shows only one mappe of each cone, and the angles  $\infty$  and  $\emptyset$  are such that two solutions, MN and M'N', are obtained. However, if one or both of the angles were greater, both mappes of the cones should be drawn, and a mappe of one cone might intersect both mappes of the other cone, which would give four solutions. If both  $\infty$  and  $\emptyset$  are 90°, there will be one solution, the common perpendicular; and the cone method would not be indicated. Obviously, if the angles  $\infty$  and  $\emptyset$  are such that the cones do not intersect, there is no solution.



#### THE NEWEST THING IN LETTERING

by

Francis W. Chamberlain and C. Ray Waddle Lincoln, Nebraska All that time is lost which might be better employed. -- Rousseau



The rapidly increasing tempo of modern industrial life accentuates the truth of this epigram. On today's drafting board, be it engineers', architects', cartographers', advertising artists' or others', more time is <u>lost</u> in that interminable task of executing acceptable lettering than in the phases of design and detail.

To minimize this profligate use of time, an amazing lettering from <u>one</u> templet has been perfected thru several years of development. With this instrument the lettering artist can easily do ten hours hand lettering in one, and a lettering novice can produce professional results almost as quickly. Its extreme functional simplicity makes it possible for anyone to letter expertly in many alphabet styles from the very first.

The outstanding feature of this device is the heretofore unknown combination of mechanical movements which makes it possible for the operator to reproduce a templet character at infinitely variable ratios of height to width. Cylindrically concave and cylindrically convex mirrors of various radii alter the reflected image in a similar fashion.

Referring to the accompanying half scale photograph:

The Varigraph Lettering Instrument is a small and compact mechanical instrument which rests on the work to be lettered and it moved. from left to right along any straight-edge. A Varigraph Lettering Templet is held under spring tension by the instrument between fixed guideways, which maintain templet alinement at all times. The engraved letter grooves in the templet are followed directly by a thumb and finger controlled stylus. Diagonally opposite the stylus the letter is reproduced at the end of the lettering arm which is raised and lowered by a finger tip controlled lever. Two scale indicating knobs are separately positionable to govern the height and width of the reproduced letter. (Continued on page 20)

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#### HEAR YE! HEAR YE!

#### ЪУ

John M. Russ Professor of Engineering Drawing State University of Iowa

It has just come to my attention that some of the plastics now used as material for drawing equipment, have the capacity for utterly destroying organic materials stored in their immediate vicinity.

Recent experience with one of these materials indicated that it had liberated fumes. These fumes attacked some adjacent drawings and records. This situation is caused by improper stabilization.

Professor Ned L. Ashton of the Civil Engineering Department at the University of Iowa, has just discovered the total loss of some very valuable inked tracings. They could not even be picked up out of the drawer. There is absolutely no question about the cause of their destruction.

Evidence indicates that some of our students' drawing instruments have been corroded after being kept in the same locker drawer with triangles and curves made out of these materials. This in spite of the fact that they were used and aired on the drawing board two or three times a week depending on class schedules.

This matter is of serious import. I think we should all know about it as soon as possible. So far as I know, or am able to find out, there is no way of telling in advance whether a plastic is of this type or not.

#### (Continued from page 19)

The templet letter being traced and the letter being produced are fully visible, as well as all previously lettered work making it impossible to smear the previously lettered work. Size changes are effected in a matter of seconds by turning the height knob or the width knob until the height and width desired are indicated on the respective scales. These scales are graduated in thousandths of an inch from one hundred and fifty to seven hundred and fifty. Lettering from one hundred and fifty to seven hundred and fifty thousand the of an inch in height or width can be made from a full size templet and lettering from seventy five to three hundred and seventy five thousandths of an inch in height or width can be made from a half size templet. Templet and instrument need not be moved to effect changes in height or width of reproduced letter. There are no adjustments of any kind to make at any time in the use of the instrument. This instrument is unique in that it can be used with equal ease by both the right and left handed person. For left handed operation rotate the

instrument ninety degrees clockwise in the accompanying photograph and slide the templet under from the edge nearest the operator.

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Lettering Templet Styles available include all the standard alphabets and many modern alphabets used today by the engineer, architect, cartographer and advertising display artist.

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(Continued from page 9)

In order to transform the spherical projection, consisting of array of points described on page 9, to a plane projection, a second operation is performed. The paper plane is first placed tangent to the unit sphere at the north pole. To obtain the "gnomonic" projection, lines are passed from the center of the sphere through the points of the spherical projection and continued until they intersect the tangent plane, to determine new points, such as  $p_G$ . To obtain the "stereographic" projection, lines are passed, not through the center of the sphere, but through the south pole, through the points of the spherical projection, and continued until they intersect the tangent plane in points, such as  $p_{st}$ .

Section and the section of the secti

The complete transformation of a typical crystal, illustrated in Fig. 2, to a spherical



Ferrous sulfate heptahydrate FeSO4.7H2O Monoclinic

Fig. 2. A typical crystal of the monoclinic symmetry class.

projection is shown in Fig. 3. The subsequent transformation of this projection to the



Fig. 3. Formation of the spherical projection of the crystal of Fig. 2.

gnomonic projection is shown in Fig. 4, and to the stereographic projection in Fig. 6.



Fig. 4. Formation of the gnomonic projection from the spherical projection.

The true shapes of these projections are then shown in Figs. 5 and 7 respectively. These



Fig. 5. The gnomonic projection showing the projection lattice and its unit cell. Note: the numbers are the "Miller symbols" of the faces (hkl). h/l and k/l are the plane coordinates of the face poles in terms of the chosen lattice.

figures should aid in the understanding of the discussion of these projections which follow.

The gnomonic projection gives us an array of points on a plane, each of which represents a crystal face and may be called a "face pole". The coordinates of each pole may be easily measured on this plane by a system of polar coordinates centered on the point of tangency, called the "center of projection". These coordinates are readily expressed in terms of  $\phi$  and p:

 $\Theta = \phi$   $r = R \tan p$ 

where R is the scale of the projection (radius of the sphere of projection). This



Fig. 6. Formation of the stereographic projection from the spherical projection.

projection has many interesting properties which strikingly express certain important properties of crystals. First, great circles



Fig. 7. The stereographic projection.

on the spherical projection become straight lines on the gnomonic projection. Thus, if a series of faces have their spherical poles on the same great circle, their gnomonic poles will all lie along a straight line. Such a series of faces, all intersecting on the crystal in parallel edges, has great significance in the study of crystals, and is called a "zone".

A second important property of crystals appears on the gnomonic projection when it is observed that face poles will always lie on the points of a regular lattice which may be superimposed on the projection. Thus, face poles in a zone will frequently appear equally spaced along the zone line. This property is a direct consequence of the Law of Rational Intercepts referred to earlier, but the law takes on much more meaning when expressed graphically in this way. When a suitable lattice is chosen to express most simply the array of face poles, the fundamental block of the lattice, called the "unit cell", is then established. Every face pole on the projection may be assigned whole number or simple fraction coordinates in terms of this unit cell. By this process, known as "indexing".



Fig. 8. The stereographic template.

a very compact and eloquent symbol (called the "Miller" symbol) is derived for any face on the crystal. It can be shown that the coordinates obtained in this way are inversely proportional to the axial intercept ratios of the crystal face. The dimensions of the unit cell have values which are characteristic of the substance forming the crystal, and the main purpose of the projection is to obtain these values. They may be read directly off the projection and compared with



Fig. 9. The two-circle goniometer. C, collimator; H, horizontal circle; T, telescope; V, vertical circle; X, crystal.

values recorded for the same substance in the literature. In the general case, five independent characteristic constants may be measured in this way, but in most cases; depending on the symmetry of the crystal, two or three are obtained.

A third property of crystals is their symmetry, which we will not have time to consider in detail here, but is really fundament. al to the study of crystals. Superficially, we will observe that if one of the symmetry elements is perpendicular to the projection plane, the projection itself will show the symmetry of that element. Thus, if a threefold rotation axis is present normal to the plane, each face pole must be accompanied by two others equivalent to it at 1200 positions around the center of projection. Axes and mirror planes frequently occur in this position, and are an important guide in the proper orientation of the crystal and classification of faces. In Fig. 5, a plane of symmetry is present on edge in a vertical position, so that the right side of the projection is the mirror image of the left side. The symmetry elements allow the faces of the crystal to be divided into groups; each group is designated by a letter, so that each letter represents a certain face on the crystal, and in addition, all the other faces present symmetrically These symmetry properties equivalent to it.



Fig. 10. Gnomonic projection and drawins of crystal of isometric symmetry class.

are illustrated for various cases by Figs. 5, 10, 12, 13 and 14.

The gnomonic projection has one great disadvantage, and that is that vertical faces on the crystal ("prism" faces) project at infinity. These faces we know have  $p = 90^{\circ}$ , so that an arrow to indicate  $\phi$  is sufficient; but very steep faces with p ranging from 75° to 90° are difficult to represent properly on the projection

The stereographic projection also consists of point face poles, but this array has



## Fig. 11. Proof of Goldschmidt's method of crystal drawing (See text).

an entirely different appearance from that of the gnomonic projection. Zones project as true circles on the stereographic projection, and thus are prominently displayed. Since spherical poles are projected along lines originating at the south pole of the sphere,



Fig. 12. Gnomonic projection and drawing of crystal of hexagonal symmetry class.

the equator projects as a finite circle (the prism zone), and all faces down to 90° are conveniently projected. But the lattice aspect of the face poles is completely lost in this projection, and this is its greatest drawback.

An interesting property of the stereographic projection is that not only great circles, but also small circles on the sphere of projection appear as true circles on the tangent plane. This gives rise to three convenient applications, as follows:

- (1) Dihedral angles on the crystal (interfacial angles), corresponding to great circle angles between face poles on the spherical projection, are conveniently measured on the stereographic projection.
- (2) The locus of face poles equidistant from a given face pole projects as a true circle on the stereographic projection. Thus, if it is known that an unknown face has an

interfacial angle 22° from plotted face A and an agle of 38° from plotted face B, these two loci are readily drawn with a compass on the stereographic projection, and the unknown face plotted at the intersection.

(3) If it is desired to rotate the crystal to a new position, the face poles are easily followed in this operation on the stereographic projection, since they move in circles. The gnomonic projection is entirely unsuited for this purpose, since the poles move in hyberbolae. The face poles may be plotted on a stereographic projection using polar coordinates by the transformation:

$$\theta = \phi$$
  $r = 2R \tan \frac{r}{2}$ 

To plot faces, and to perform the operations described above, it is convenient to use a template on which the transformed angles are permanently graduated. The most convenient template is one shown in Fig. 8, in which a system of great circles is projected intersecting in a horizontal axis, and a system of small circles projected normal to the same axis. The crystal projection can then be made easily on tracing paper over the template, arranged to rotate freely about a pin at the center.

#### PROCEDURE FOR CRYSTAL MEASUREMENT

It appears, then, that suitable combination of these two projections in the process of analyzing a crystall will satisfy all the needs of the crystallographer. We may now follow a typical morphological analysis of a crystal, to see how they are applied.

The first practical problem is the measurement of the crystal. The classical instru-ment for this purpose is the simple contact goniometer (arm and protractor), used by Hauy, and still used today for large, hand sized crystals. This device measures, with say  $\pm \frac{1}{2}$ accuracy, the dihedral angles between the faces of the crystal. A refinement of the method was developed in the one-circle goniometer, which is adapted to the measurement of much smaller crystals with an accuracy of  $\pm \frac{1}{6}$ minute of arc. It consists of a horizontal graduated circle on which the crystal is mounted and rotated. A collimator and telescope are fixed to the stand supporting the rotating circle, with their horizontal optic axes intersecting the vertical axis of the circle. The observer sees a signal formed by a reticle in the collimator when a crystal face, acting as a plane mirror, is in position to reflect it into the telescope. To measure the angle between two faces, it is necessary to orient the crystal so that both faces are vertical. Each face is then brought into

reflecting position, and the angles read on the graduated circle at these positions provide by their difference the dihedral angle. To measure other dihedral angles, the crystal must be reoriented for each zone.

More useful data are obtained by use of the two-circle goniometer shown in Fig. 9. This instrument is based on the one-circle goniometer, but a second, vertical, graduated circle is mounted on the horizontal one, so that the crystal, attached to the vertical circle, lies at the intersection of the two circle axes, and the optic axes of the collimator and telescope. The two circles now correspond to the two spherical angles  $\varphi$  and p. By proper adjustment of the two circles, any face on one hemisphere of the crystal may be brought into reflecting position, without remounting the crystal. When a face is in this position, its angle of inclination (p)may be read directly on the horizontal circle, and the angle of azimuth ( $\phi$ ) on the vertical circle. With this instrument, a crystal as small as 1/20 millimeter may be precisely and completely measured in one setting.

The next step in the process is the plotting of the stereographic projection of the crystal from the data obtained with these instruments. Where dihedral angles only are available, as obtained from the one-circle goniometer, the projection must be constructed by laying out spherical triangles on the template by the use of circle loci, until all the zones are located. Where spherical angles are available, as obtained from the two-circle goniometer, they may be plotted directly by use of the transformation formulae suggested above, or better by use of the template. Thia projection may now be rotated in various ways until it is brought into a standard position with respect to symmetry and well-established conventions. If this orientation is known beforehand, the crystal can be set up on the two-circle goniometer so that the resulting projection will automatically have the right orientation. In this case, the face poles may be plotted immediately on a gnomonic projection without using a stereographic projection. Fortunately, this is the common circumstance. But when it is not, the stereographic projection is used to achieve the correct orientation; when this is done, the reoriented face poles are then transferred to a gnomonic projection.

In any case, a gnomonic projection of the crystal in its proper orientation is obtained by one route or another. On this plot, the basic lattice on which the face poles lie is usually obvious. The choice of lattice is always somewhat ambiguous, since there are always two or three possible unit cells, among which it is impossible to choose, except arbitrarily. As we have seen, the lattice dimensions, measured directly on this projection, are characteristic of the substance (Continued on page 26)

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#### A NON-CREDIT COURSE IN DRAWING IN LIEU OF HIGH SCHOOL DRAWING FOR STUDENTS DEFICIENT IN HIGH SCHOOL DRAWING

by Robert R. Irwin

Assistant Professor of Mechanical Engineering, Oklahoma A & M College, Stillwater, Oklahoma

Fortunately or unfortunately, not all students enter a college of engineering with the same background. In the same vein, not all graduates attain the same level of training and knowledge. Between the minimum and maximum levels stands the engineering instructor with his pencil poised to outline a course of study for Engineering Drawing. Which level do you choose? Sitting on the fence merely makes you the target for both sides. On one side the student who does not know what a T-square looks like, on the other, a student with four years of high school training.

A survey of students enrolled at present in the School of Engineering at Oklahoma A & M College disclosed that 60% had not taken a drawing course in high school, 18% had taken a single semester of drawing, and 22% had more than one semester high school training in drawing.

Approximately 25% of Oklahoma high schools offer courses in drawing. Of course, most of the larger schools that furnish the largest percentage of students for the Engineering college offer several courses in drawing. It is probable that over half of the engineering students have an opportunity to take drawing in high school.

May I describe the situation of the basic Engineering Drawing course in the Engineering college. With variations, the situation at Oklahoma A & M College is much the same as at most other engineering schools. A two credit hour course in basic engineering drawing is offered and required of all engineering students except those enrolled in the School of Architecture. There are no prerequisites for the course. An advanced machine drawing course is required of students in the Department of Mechanical Engineering. This means that the majority of students receive their only training in drafting from courses in Engineering Drawing and Descriptive Geometry.

The objective and traditional purpose of these courses is to give the student the ability to use and understand the language, drawing. Courses in the oral and written language are utilized throughout a student's formal education. Even the most hopeless appearing freshman can write home for money. Consider the contrasting background of engineering students in the two languages.

My purpose today is to urge more adequate backgound for students in the language of drawing. I agree most heartily with Professor John Rule's statement in this article <u>Graphics Re-Examined</u>. "It is difficult to visualize how lost the engineer would be if he had no acquaintance whatever with the drawing board." This acquaintance must be started earlier than is now the general practice if the first year courses in graphics are to make possible, the "ultimate stature of Scientific and Engineering Graphics" envisioned for them by men who have contributed so much to their present stature. The logical place to start this earlier acquaintanceship is in the high school by requiring 1 credit or  $\frac{1}{2}$  unit of drawing as a college entrance requirement.

From the previous discussion it is apparent that regardless of how worthwhile the objective of requiring drawing in high school, the engineering college will have to help solve the problem. A non-credit course could be set up that would enable entering students without high school credit to meet the entrance requirement. Under such a scheme, the prerequisite for the Basic Engineering Drawing course would be the entrance requirement of 1 credit in high school drawing or the elementary drawing course. The immediate benefit of an elementary drawing course to students in Basic Engineering Drawing, is that the student will be able to start his study at a higher level and his progress should allow fuller attainment of the course objectives. A secondary benefit that might prove to be the most important, would be the introduction of drawing as a general educational subject. Certainly in a technological age such as ours, all members of society are beginning to feel the need of a knowledge of the language of drawing.

One objection to requiring the elementary drawing course or its equivalent would be that the time required for graduation might be increased. This objection is not valid however, as only about 25% of graduating students are able to obtain their degree in eight semesters. Of course as the demand for a high school drawing course increases, the number of schools offering such a course will increase and the problem will gradually become one for the high school and not the college.

I feel that it is necessary for the college drawing instructors to cooperate with the schools training high school drawing teachers and with the teachers themselves in order that the entire level of instruction in engineering drawing may be raised. Many high schools do not include drawing because due to various factors they are able to maintain only a minimum level of courses offered. Requiring drawing for college entrance will serve as a device to introduce or increase training in the graphical language.

The elementary drawing course should stress the fundamentals of drawing and leave to the Basic Engineering Drawing course the problem of composing working drawings. The subjects that should be stressed in such a course are as follows:

> Proper use of instruments and materials. The geometry of engineering drawing Projection. Sectioning. Introduction to dimensioning. Introduction to fasteners.

Naturally there will be as many different groupings of the above list as there are people discussing the idea. The suggested time allowed for such a course would be the equivalent of one semester credit hour, or three hours of class work each week. This amount of time would probably be adequate to give a course equivalent to a single semester of high school work.

#### A REPORT OF THE VISUAL AIDS COMMITTEE

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bу

#### H.B. Howe, Chairman Rensselaer Polytechnic Institute Troy, New York

The aims of the committee:

- (1) To survey the various visual aid methods. (the committee decided to limit its survey at this time to film, film strip and slides.)
- (2) To publicize a summary of the survey.
- (3) To investigate and promote further development of effective visual aid methods.

The committee mailed 335 questionaires and received 156 replys, with 44 answers indicating visual aid users. The accompanying map shows the distribution of the above information.

Comments and inquiries indicate membership consciousness of the impetus this type of teaching aid gives to a fuller inspirational lift and understanding of fundamental and related subject matter. However, it is obvious that with the list of films available (table #3), the finding of this survey does not impart a finished picture of the aids now in use. We apparently have not contacted all of our members who use them. In order to give a truer picture we ask each additional, present or new user of visual aids to send information that we may make our survey more complete.

The committee appreciated the cooperation of the members in conducting this survey.

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		Warner		

#### (Continued from page 24)

Visual Aids Committee

forming the crystal, and may be used to identify that substance. In the case of minerals, the lattice constants of all species have been tabulated in complete form, and an unknown crystal may usually be identified by comparing the graphically determined constants with



#### VISUAL AID SURVEY Distribution Map

Key:

Questionaire

+ reply received

O- visual aids user

-12 school no. (see table #2)

Rensselaer Polytechnic Institute A & M College of Texas Illinois Institute of Technology University of Minnesota Syracuse University Purdue University General Motors Institute University of Washington

these tables. These lattice constants are identical, incidentally, with those determined unambiguously by X-ray diffraction methods.

Both the stereographic and gnomonic projections may be used to determine readily (Continued on page 28)



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interfacial and interzonal angles, and the geometry of any other vectorial properties of the crystal (e.g. optical properties). These measurements may be refined by mathematical and statistical analysis of the original data if desired. It is a curious fact, however, that the average deviation of carefully made goniometer measurements (seldom as good as 0.1%), with rare exceptions far exceeds the magnitude of accuracy ordinarily claimed for lattice measurements (0.01%). Crystals are never perfect creations, except by the crudest standards.

#### CRYSTAL DRAWING

Finally, in our procedure of morphological analysis, we find that drawings of the crystal in orthographic projection along any desired projection direction may be made directly and easily from the gnomonic projection. Goldschmidt's method for doing this, illustrated in Fig. 10, is ingenious and striking. Let us first follow the procedure itself; it is simply stated as follows:

- (1) An orthographic projection plane (picture plane) is passed through the center of the sphere of projection, in any desired orientation. It is identified by its trace on the gnomonic projection plane, a straight line which we shall call the "guide line". The position of this line immediately indicates the orientation of the picture plane.
- (2) The picture plane is rotated into the gnomonic plane about the guide line as an axis. The center of the sphere is readily found in its rotated position, and this point is called the "angle point".
- (3) If two faces intersect on the crystal, their face poles are joined by a straight zone line, which is extended until it intersects the guide line.
- (4) The intersection point found in step (3) is joined by a straight line with the angle point. The direction of the line into which the edge between the two faces will project on the picture plane is normal to this line.

By this simple process, any desired picture plane may be immediately established, and the edge between any pair of faces on the crystal may be quickly and easily constructed upon it. The shape of the crystal and its faces is determined as the drawing proceeds by reference to another drawing, or better, the original crystal. Thus the third dimension is reintroduced, as it cannot be supplied by the gnomonic projection. When it is desired to draw a crystal in ideal form with respect to its symmetry, many crystallographers find it convenient to draw a plan of the crystal where the axes and planes of symmetry appear on end and on edge. In this case, the picture plane is the gnomonic projection plane, and the crystal edges are simply drawn normal to the corresponding zone lines themselves. In this view, the faces of the crystal can be accurately drawn in their proper size and shape. The usual pictorial orthographic is then drawn on a conventional picture plane with  $p = 80^{\circ}$  and  $\phi = 70^{\circ}$ . The proportions are maintained accurately in the pictorial view by direct projection from the plan view. Thus, the pictorial (which, though strictly orthom graphic, is often called "perspective" by crystallographers) gives an attractive view from a point of view, so to speak, 10° above and 20° to the right of the crystal. As a matter of fact, in the drawing of this pictorial, the operations of symmetry can be followed in this view directly as a guide to the ideal development of faces, so that the plan view is unnecessary, and best omitted.

It would be worthwhile, perhaps, to verify the rather extraordinary construction just described with a simple geometric proof. In Fig. 11, let the face poles s and t on the gnomonic plane G be given, and the picture plane P. All lines and planes will be drawn through the common point 0, the center of the projection sphere. The intersection line between the crystal faces represented by vectors Os and Ot will be parallel to line Oc, which is perpendicular to plane Z containing lines Os and Ot. Line Oc will be projected orthographically onto plane P into line Ob by plane W, perpendicular to plane P. In the construction, the zone line st on the gnomonic projection plane G is extended to cut the trace of plane P in plane G (the guide line) at point a. Line Ob is then constructed normal to line Oa (with the plane P rotated into the paper plane G). We would like to show that Ob is truly perpendicular (Continued on page 30)

# TECHNICAL DESCRIPTIVE GEOMETRY PROBLEMS

b y

WILLIAM E. STREET

Produces and Hoad of the Engeneering Drowing Department, Agricultural and Washmical Colleger of Fusios

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Published in August, 1947, the problems in this text are organized for use with any suitable text book although designed with a view towards Professor Street's forthcoming book <u>TECHNICAL DESCRIPTIVE GEOMETRY</u>. They have been selected to emphasize descriptive geometry fundamentals applicable to all technical fields. Methods of solution have been painstakingly correlated with industrial drawing methods as set forth in all standard works on Engineering Drawing. It is for the generally accepted freshman course.

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(Continued from page 28)

to Oa. Plane W will contain line Oc, normal to plane Z, and line Od, normal to plane P. Since line Oa lies in both planes Z and P, it will be perpendicular to both lines Oc and Od, and therefore, perpendicular to plane W. Therefore, line Oa will be perpendicular to line Ob, which lies in plane W.

Drawings can also be made very conveniently directly from the stereographic projection. Fig. 13 shows an example illus. trating the method, which is similar in



Fig. 13. Stereographic projection and drawing of crystal of orthorhombic symmetry class.

principle to that used with the gnomonic projection. The picture plane is first established in any desired position by drawing the projected great circle in which it cuts the projection sphere (long-dashed circle in the figure). The zone circle between two poles, such as x and n, is extended to cut the picture plane circle. This point of intersection determines a line with the center of . the sphere which corresponds to line a0 in Fig. 11, and is perpendicular to the desired projected crystal edge between faces x and n. The picture plane is now rotated into the paper plane about a horizontal axis, and the normal constructed to the radial line as shown.

Crystals often grow in pairs called twins, in which one individual is related to the other so that it is the mirror image of the other over a possible crystal face as a twin plane. Fig. 14 shows such a twin with its stereographic projection. The faces of





the upright individual are projected as circles, the twin plane as a dotten circle with its pole at e, and the faces of the twin individual as triangles. The last are readily constructed from the first, as shown by ? as an example. ? and its twinned counterpart? lie in a zone with the twin plane e, and the angle  $? \land ?$  is bisected by the twin plane. It is seen, then, that the important phenomenon of twinning of crystals is easily handled quantitatively by projection methods.

Crystal drawing is thus so highly developed that it is possible to make the most complex crystal drawings by routine methods, without regard to theory. In a way, this is fortunate, for it is a curious fact that very few crystallographers are good draftsmen or expert in graphical methods; Goldschmidt's methods enable such workers to carry out drawings by rote. On the other hand, rote methods are dangerous here as in any process, for in the hands of persons who depend on rote they lead to unsuspected errors and inaccuracies which occasionally are rather serious. In the hands of a crystallographer thoroughly familiar with the principles behind the projection methods and also general descriptive geometry and drafting techniques. however, the methods are very powerful, rapid and accurate.



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(Continued from page 15)

The American Standards for graphical symbols and abbreviations for use on drawings, has proposed a symbol similar to the square root sign ( $\sqrt{}$ ) to indicate the finish of a surface. The addition of a numerical symbol in the opening of the "V" portion would denote the qualitative value of the roughness permitted, measured in microinches. When specifying the roughness symbol on a surface, one should remember to specify only the surface requiring special accuracy, because of extra cost involved.

The following table has been prepared by the American Standards Association and gives the roughness symbol and the root mean square values of surface irregularities for the most commonly used designations for surface specifications:

Rough- ness Symbol	Root Mean Square Height of Irreg- ularities (Inches)	Microinches
63M	.063	63000
16M	.16	16000
4M	.004	4000
1M	.001	1000
250	.00025	250
63	.000063	63
32	.000032	32
16	.000016	16
8	.000008	<b>8</b>
4	•000004	4
2	•000002	2
1	•000001	1
	.0000005 .00000025	고 양 년

The surface roughness symbol as specified in the first classification, (62M, 16M, 4M, and 1M), applies to surfaces produced by rough machining, turning, boring, and milling. This group also applies to rough castings that have been thoroughly cleaned of all sand and scale.

The increasing demand for higher output and smaller clearances in the internal combustion engine, necessitates the use of the second group of roughness symbols for critical surfaces. For example: 250, 63, 32, 16, and 8, would be used on surfaces such as pistons, crankshaft bearings, connecting rod bearings, and valve stems. Diamond boring and finish grinding are also included in this series.

The third classification 4, 2, 1, is for very fine finishing operations, finish grinding followed by polishing, and lapping. Current manufacturing processes, at the present time, approach this series. The fourth classification  $\frac{1}{2}$ ,  $\frac{1}{4}$ , etc., applies to highly polished finishes used largely in experimental laboratories and on gauges.

Although the American Standards Association has proposed the placing of the roughness symbol on the surface to be controlled, the industries have found it more convenient to specify it in the form of a note. This can be appreciated by the fact that most drawings are very crowded without the addition of roughness symbols on all critical surfaces; furthermore, by placing the surface specification in a note, it is not likely to be overlooked.

Figure II shows a valve and valve guide which illustrates a method of designating surface control without the use of symbols.



FINISHED WITHIN 80-120 MICEDINCHES (2.M.G.) VALVE GUIDE

The diameter and a note specifying surface roughness would be shown in a similar manner on the valve.

Figure II

It is interesting to note that the variation of surface finish between 80 and 120 microinches is important in this case to insure lubrication by the proper functioning of the valve and the valve guide. If the two surfaces were held to closer limits, 10 to 50 microinches for example, there would be a pumping action between the valve guide and the valve stem. However, if the two surfaces were permitted to be finished to wider limits of roughness, 150 to 200 microinches, there would be very poor lubrication between the two parts. It is obviously apparent that surface specification is important and necessary in order to produce specific results demanded by industry.

Roughness specifications are also used on the outside diameter of pistons, because of the increase in compression ratio and reduction in the clearance between the pistons and cylinder walls.

These examples represent the trend in surface quality specification by some of the largest industrial plants in the country. (Continued on page 34)

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